

Order designation

	LZR 2025-38.20-16
System designation	
Mounting profile	
Clamping profile	
Timing belt width	

Sample order

Linear module	LZR 2025-38.20-16
Item no.	B38.25.001
Stroke	=mm
Length	L =mm
Roller carriage length	L1 =mm
Drive shaft borehole	ø =mm
Travel speed	v =m/s
Acceleration	a =m/s ²

Linear Modules LZR

Linear modules with timing belts (LZR) have a modular design and are installed on the track roller assemblies. Their basic components include the mounting profile, profile guide and carriage plate and the timing belt drive components required to transmit power, such as the pulleys and connectors.

The LZR design facilitates the attachment of motors as standard. With the appropriately drilled shafts, the pulleys allow the motor to be attached directly on any side. In addition, shaft ends for flanged mounting of a gearmotor with a hollow shaft, adaptations with a motor flange and coupling and an indirect drive are available on request.

For electromotive drives using a stepper motor or servomotor, we recommend using the optional single-piece drive shafts.

The linear modules can be combined in two-axis and three-axis systems and in area gantries and three-dimensional gantries.

Level of Accuracy that can be achieved by Linear Modules with Timing Belts

The LZR with a 8M-30-type timing belt can achieve the following values without a load:

Repeatability:		0.1 mm
Positioning accuracy:	±	0.2 mm
Reversal error:		0.2 mm

These values vary depending on the stroke length and application.



Notes on the Load Specifications

For information about load specifications for track roller assemblies, refer to the information beginning on page 42.

Notes on the Load Specifications for Timing Belts

The standard timing belts used are PU (polyurethane) with steel cord tension members. Other types, including conductive belts, are available on request.

The maximum track roller assembly travel speed of v = 10 m/s can be achieved using timing belts with no reduction of the load capacities.

From a > 10 m/s² onwards, the values must be reduced by the usual load factors (e.g. without load peaks s = 1 to high load peaks s = 2.5).

The allowable tension loads are based on a 0.4% elongation of the timing belt.

The breaking strength of the belts is significantly higher. The normal usable belt pull strength (Fu) and required pretension (Fv) is approximately:

 $F_{allowable} = F_v + F_u$ with $F_v = F_u$

Timing Belts	AT 5-16	5M-15	8M-30
F _{breaking}	3900 N	3600 N	14900 N
F _{allowable}	1200 N	1150 N	4000 N
$F_v = F_u$	600 N	575 N	2000 N

The usable starting torque results from the maximum usable belt pull strength, of the engaged teeth and the pitch diameter of the timing belt pulley.

The values for the mk LZR modules are:

Timing belt	AT 5-16	5M-15	8M-30
D _{Pitch}	41.4 mm	50.9 mm	71.3 mm
Z	26	32	28
M _{Drive}	12 Nm	15 Nm	70 Nm

Motor Selection/ Drive Design

For the drive selection, several factors must be considered, including the timing belt (especially the allowable belt pull strength and required stiffness) and the motor (especially the starting torque, the revolutions per minute and the resulting performance). The most important consideration is the required driving force. As a simple starting point for the calculations, the transition point from acceleration to constant speed can be used.

Constant acceleration

(a = constant):

 $v = a \cdot t = \sqrt{2 \cdot a \cdot s}$

Constant speed (v = constant):

Max. driving force:

 $F_{Drive} = F_a + F_{Roll} + F_{Empty} + F_{Additional}$ $F_a = m \cdot (a+g)$

- with m = moving mass in kg
 - a = const. acceleration in m/s²
 - $g = 10 \text{ m/s}^2$, for vertical travel
 - $g = 0 m/s^2$, for horizontal travel

 $F_{Roll} = F_N \cdot \mu_{Roll}$

with $F_N = F_G$ for horizontal travel $\mu_{Roll} = 0.05$ for lightly preloaded track roller

 F_{Empty} = 50 to 100 N depending on the module and pre-tension of the timing belt

 $F_{Additional}$ = additional loads from the application F_{Drive} = m · (a+g) + FN · 0.05 + 100 N + $F_{Additional}$

For timing belt selection:

Indicated F_{Drive} < F_u

For motor selection:

$$\begin{split} \mathsf{M}_{req} &= \frac{\mathsf{F}_{\text{Drive}} \cdot \mathsf{D}_{\text{Pitch}}\left[m\right]}{2 \cdot \eta} \\ \mathsf{n}_{req} &= \frac{\mathsf{v} \cdot 60}{\mathsf{D}_{\text{Pitch}}\left[m\right] \cdot \pi} \\ \mathsf{P}_{req} &= \frac{\mathsf{F}_{\text{Drive}} \cdot \mathsf{v}}{\eta} \end{split}$$

With D_{Pitch} in m of timing belt pulley η = 50 too 75% depending on selected drive (gearbox, motor, etc.) v in m/s

Linear Modules LZR



Load Specifications for LZR 2000-38.41-15 with Plate Carriage

	L1	Fx**	F _{y0}	F _{z0}	M _{x0}	M _{y0}	M _{z0}
Item no.	[mm]	[N]	[N]	[N]	[Nm]	[Nm]	[Nm]
B38.02.003	150	1150	1000	2000	25	100	50
B38.02.003	250	1150	1000	2000	25	200	100

* Maximum stroke between the mechanical stops. Note the discharge section!





	L1	Fx**	F _{y0}	F _{z0}	M _{x0}	M _{y0}	M _{z0}
Item no.	[mm]	[N]	[N]	[N]	[Nm]	[Nm]	[Nm]
B38.02.007	250	1150	1000	2000	25	200	100

* Maximum stroke between the mechanical stops. Note the discharge section!

** $F_x = F_{allowable}$; $F_u = 575 \text{ N} = F_v$



Load Specifications for LZR 2004-38.41-30 with Plate Carriage

	L1	Fx**	F _{y0}	F _{z0}	M _{x0}	M _{y0}	M _{z0}
Item no.	[mm]	[N]	[N]	[N]	[Nm]	[Nm]	[Nm]
B38.02.004	150	4000	1000	2000	25	100	50
B38.02.004	250	4000	1000	2000	25	200	100

* Maximum stroke between the mechanical stops. Note the discharge section!





Load Specifications for LZR 2004-38.44-30 with Side Mounted Plate Carriage

	L1	Fx**	F _{y0}	F _{z0}	M _{x0}	M _{y0}	M _{z0}
Item no.	[mm]	[N]	[N]	[N]	[Nm]	[Nm]	[Nm]
B38.02.005	250	4000	1600	4000	80	350	150
B38.02.005	450	4000	1600	4000	80	760	300

* Maximum stroke between the mechanical stops. Note the discharge section!



Load Specifications for LZR 2005-38.44-30 with Plate Carriage

	L1	Fx**	F _{y0}	F _{z0}	M _{x0}	M _{y0}	M _{z0}
Item no.	[mm]	[N]	[N]	[N]	[Nm]	[Nm]	[Nm]
B38.02.006	250	4000	1600	4000	80	350	150
B38.02.006	450	4000	1600	4000	80	760	300

* Maximum stroke between the mechanical stops. Note the discharge section!





Load Specifications for LZR 2005-38.44-30 with Side Mounted Plate Carriage

	L1	Fx**	F _{y0}	F _{z0}	M _{x0}	M _{y0}	M _{z0}
Item no.	[mm]	[N]	[N]	[N]	[Nm]	[Nm]	[Nm]
B38.02.009	250	4000	1600	4000	80	350	150
B38.02.009	450	4000	1600	4000	80	760	300

* Maximum stroke between the mechanical stops. Note the discharge section!

Linear Modules LZR



Load Specifications for LZR 2011-38.44-30 with Plate Carriage

	L1	Fx**	F _{y0}	F _{z0}	M _{x0}	M _{y0}	M _{z0}
Item no.	[mm]	[N]	[N]	[N]	[Nm]	[Nm]	[Nm]
B38.02.011	250	4000	1600	4000	80	350	150
B38.02.011	450	4000	1600	4000	80	760	300

* Maximum stroke between the mechanical stops. Note the discharge section!





Load Specifications for LZR 2011-38.44-30 with Side Mounted Plate Carriage

	L1	Fx**	F _{y0}	F _{z0}	M _{x0}	M _{y0}	M _{z0}
Item no.	[mm]	[N]	[N]	[N]	[Nm]	[Nm]	[Nm]
B38.02.010	250	4000	1600	4000	80	350	150
B38.02.010	450	4000	1600	4000	80	760	300

* Maximum stroke between the mechanical stops. Note the discharge section!



Dual VST 2015 with coupling via timing belts for width adjustment of the ZRF-P 2040.02 cycle conveyor



System 2015 adjusting units with handwheel and scale



Dual VST 2015 with manual digital display for adjusting the stop bar





Dual electromotive VST 2015 for automatic width adjustment with scanning via safety limit switch

Electromotive VST 2015 with recirculating ball bearing guide



Dual VST 2015 with parallel recirculating ball bearing guide for supporting the load



Manual two-axis adjustment system for holding a marking device with VST 2015



Dual VST 2011 for manual lane width adjustment on a side conveyor



Electromotive VST 2011 with custom measuring system on LZR 2005-38.44-30



VST 2011 adjusting unit used for semi-automatic conveyor width adjustment in a chain conveyor system





VST 2011 with two counter-rotating slide carriages and digital display for adjusting the width of the pneumatic centring unit on the modular belt conveyor



System mk 2011 adjusting unit for brush cantilever



VST 2011-H with handwheel as add-on kit for the belt conveyor with incline adjustment



Horizontal slides comprised of linear module type LZR 2005-38.44-30 with fork grippers and swivel unit for moving and emptying workpiece baskets



Double-LZR 2005-38.44-30 with side mounted carriage plate and cantilever for conveyor as lift



Linear module type LZR 2005-38.44-30 as a direct length measuring system with measuring head on the roller carriage





Pneumatic linear module with PF 38.77 and LW 38.77-44 as a transfer unit with 10 vacuum suction grippers





Linear unit LZR 2004-38.41-30 drive coupled via a slip clutch



Linear unit LZR 2004-38.41-30 as a height adjustment unit for an assembly and testing workstation



LZR Series 60 linear module based on the mk 2060.07 profile with track rollers and rails from Rollon





Linear module with chain for HT range and in ESD version Product intake with pneumatic lift for lifting/depositing before, in and after the oven



Gantry with LZR 2005 on foamed combined profile Roller carriage with support rollers as cross-carriage with LZR 2005 and Omega drive as X-Z surface gantry





Linear module type LZR 2005-38.44-30 with motor and controller as a lift with a belt conveyor



Base LZR 2005-38.44-30 with side roller carriage on foamed combined profile as gantry, with support rollers for torque loads and manual VST 2011 as Z axis



Linear module type LZR 2004-38.41-30 with absolute value rotary encoder mounted on the tail



Dual LZR 2005-38.44 with cantilever for dual ZRF-P 2010 for lift and transfer from a dual ZRF-P as a lift-and-transfer module



LZR 2004-38.41-30 with servo gearmotor from Infranor



Dual-axis linear module comprising LZR 2011-38.44.30 with side mounted carriage plate





Dual LZR 2005 as lift in steel rack

Dual linear module type LZR 2005-38.44-30 with cantilever for conveyor as a lifting unit



Three-axis gantry with driven linear modules, gripper and controller



Two-dimensional gantry with vacuum gripper as a handling and loading system for steel. Two independent loading systems on a common X axis with gear rack with track rollers and riding rack drive



X-Z axis combination with pneumatic drive and vacuum grippers for loading and unloading beverage crates



X-Z gantry with gripper for transferring crankshafts. X axis as LZR with support roller and timing belts, Z axis with timing belt Omega drive and fall arrest









Horizontal axis with foamed combined profile for reinforcement



Gantry stand with telescopic gripper unit



Short stroke lift based on PF-38.44 linear guide system



X-Z gantry with additional pneumatic weight balancing as a holder for a vacuum gripping system



Lift station for lifting and lowering conveyors on two conveyor levels. Cross-conveyor unit with recirculating ball bearing guides positioned horizontally in the frame



Recirculating ball bearing guide for manual lane width adjustment and for clamping the pneumatic centring device and electromotive rotating unit





Lifting unit with KU 25 recirculating ball bearing guide and angle bracket





Frame for stress testing based on KU 30.10 recirculating ball bearing guide



Shuttle system with rotary indexing table for pallet transport, guided via a double linear axis with recirculating ball bearing guide



Gantry for handling sleeves. The X axis is moved by a dual linear module with a KU 30.30 recirculating ball bearing guide



Two-track feed for machine loading. The separator can be adjusted for various diameters using a recirculating ball bearing guide



Lifting unit with LZR with recirculating ball bearing guide KU 25 with profile cantilever for supporting the ZRF-P 2010 conveyor





Timing chain conveyor with alignment unit for camshafts using recirculating ball bearing guide





LZR with recirculating ball bearing guide



Transfer shuttle with pallet carriers, carriage with recirculating ball bearing guide